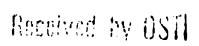
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TITLE NONDESTRUCTIVE ASSAY OF PLUTONIUM BEARING SCRAP AND WASTE WITH THE ADVANCED SEGMENTED GAMMA-RAY SCANNER

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# NONDESTRUCTIVE ASSAY OF PLUTONIUM BEARING SCRAP AND WASTE WITH THE ADVANCED SEGMENTED GAMMA-RAY SCANNER

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#### **ABSTRACT**

Assaying plutonium-bearing scrap and waste (S&W) for plutonium content can be very difficult because of the heterogeneous nature of the items. Previous efforts have been hampered by the lack of representative standards for calibrating and evaluating measurement performance on actual plant materials. We have characterized 25 S&W items in three distinct S&W categories to 2% or better. We used these items with fabricated calibration standards to evaluate the performance of the lump-corrected segmented gamma-ray scanner. We show that some difficult-to-measure S&W samples can be assayed with less than 10% bias, but still suggest that each category of S&W be individually evaluated for measurement bias.

#### INTRODUCTION

All nuclear material processing facilities generate large amounts of heterogeneous scrap and waste (S&W) containing special nuclear material (SNM). This scrap and waste needs to be measured to compute the material balance. (We define scrap as material with sufficient SNM to make recovery economically viable; waste does not have sufficient SNM for recovery.)

Most chemical techniques rely on sampling the item and then extrapolating the results from the sample to the original item. For heterogeneous scrap and waste, chemical analysis is not viable because of the difficulties of obtaining representative samples; these samples have traditionally been measured by nondestructive assay (NDA) instruments. NDA has some advantages compared to chemical analysis; it measures the entire sample, the sample does not have to be homogenized, it does not generate more waste, and it is easier to apply. However, NDA is not the answer to all assay problems; some waste, for example, large crates, cannot be measured quantitatively by any means.

This paper describes the capability of the advanced segmented gamma-ray scanner (SGS) to measure a wide variety of plutonium-bearing scrap and waste. Real samples were obtained from operating facilities and subsequently carefully characterized. The samples include low-density plutonium bearing ash, high-density plutonium oxide, sand-slag crucibles (SSC), and salts generated from the molten salt extraction (MSE) process. This paper demonstrates that some of these process samples can be measured quite well with the state-of-the-art techniques on the SGS.

## **PRINCIPLE**

The SGS¹ was developed in the 1970s for low-density, reasonably uniform samples. The SGS assay is based on the 413-keV gamma ray spontaneously emitted from <sup>239</sup>Pu. Corrections are made for rate-related counting losses and the attenuation from sample matrix self-absorption. The sample is viewed in slices or segments defined by moving the sample vertically, in discrete steps, in front of a collimated detector. The segmentation reduces the bias caused by vertical heterogeneity in the sample. The samples are rotated during the assay, which tends to reduce the effects of horizontal heterogeneity.

Assay results, however, can still be biased (nearly always low) if the density of the sample is high or if the sample contains lumps of plutonium. Recent improvements in SGS analysis started with improving the matrix attenuation correction factor, and volved into correcting for the presence of the lumps.<sup>2</sup> These improvements can be summarized as follows:

- Quadratic interpolation of the measured transmission to deduce the sample transmission at the assay energy rather than use the transmission measured at the transmission source energy.<sup>1</sup>
- 2. Calculation of the attenuation correction factors using numerical integration of actual sample/standard geometry instead of the far field approximation. Polynomial functions are used to fit the correction factors as a function of the transmissions. This improvement reduces some of the correction factor errors for homogeneous samples from between 5% and 10% to 1%, using numerical integration as the reference and benchmarking with measurements on standards.
- 3. Assays for plutonium are performed at several energies, and the suppression of the lower energy assay is used as an indicator of the presence of lumps of SNM in the sample. A lump correction is performed based on the assumption that the lumps are spherical and of the same size.<sup>2</sup>

These improvements in the data analysis are the main features of the advanced SGS. To test its validity, the instrument was used to assay a group of well-characterized process samples whose SNM contents are characterized to 2% or better by methods described below. The results of the advanced SGS assays are compared with a neutron coincidence counter (NCC). Traditionally, for the plutonium bearing S&W, we

suspect the results from the NCC are biased high, and that the SGS results are biased low. This can be used, in most cases, to bracket the true result.

#### **CALIBRATION**

The advanced SGS was calibrated with the standard STDASH-1; the calibration was validated with STDASH-2. Both of the STDASH standards are fabricated from plutonium oxide and diluted with diatomaceous earth. We have found these standards to be uniform and homogeneous. The particle size distribution of each standard is not known.

The NCC was calibrated with the PEO and LAO series of oxides. The PEO samples are prepared with 10% <sup>240</sup>Pu ranging from 20 g to 780 g of plutonium; the LAO samples are prepared with 16% <sup>240</sup>Pu and with plutonium masses ranging from 60 g to 870 g. The plutonium contents of these standards were determined from the chemical preparation and recently validated with calorimetry and gamma isotopics. These standards are intended for the NCC; in general they are too dense for the SGS and fairly opaque for gamma-ray transmission at the assay energy. They mimic clean scrap.

## **RESULTS**

The results are summarized in Table I for both instruments.<sup>3</sup>

The first set of samples measured consists of plutonium-bearing ash with a relatively low density (~0.5 g/mL) from Hanford. These samples are appropriate for the SGS because they are low-density waste that is fairly uniform. Figure 1 shows the SGS assay results. The SGS assays have a relative standard deviation (RSD) of 0.7%, which is approximately the precision of the measurements with very little bias. In comparison, the NCC assays of these samples fluctuate substantially more with an RSD of 5%.

The second set of samples consists of the plutonium oxide. Although these samples have a relatively high density and should be measured by NCC, they were measured with SGS for completeness. The results are shown in Fig. 2. In general these samples are too dense for the SGS and fairly opaque for gamma-ray transmission at the assay energies. The NCC assay results have an RSD of 3% while the SGS assay results fluctuate with an RSD of 24%. The average SGS result is only 6% low: probably a fortuitous result of sample geometry.

Sample ID	Reference (g Pu)	906 (g. Pu)	Sigma (%)	SGS/Reference Ratio	NCC (g. Pu)	Sigma (%)	NCC/Heiurence Ratio	NCC & SGS Average	Av/Reference
Seripic ID	W 1-01	W 507		MAIIV	(M.FV)		rieno	-	7400
ow-density Ask									
STOASH . 1 *	20.09	20.91	0.45	0.998	20.13	1.60	0.959	20.52	0.977
STDASH - 2 *	20.95	21.08	1.41	1.005	20.17	1.77	0.983	20 62	0 984
ASH 685-003	33,14	32.98	0 84	0.935	32.53	3.05	0.981	32.75	0 988
ASHHVA - 27	51.30	52.03	0.36	1.014	49.22	4.11	2.959	50.62	0.987
ASHHVA - 5	104.95	164 94	0.43	1.000	178 61	5 00	1 071	170 78	1 035
ASHHVA - 6	8.70	0.72	1 81	1.004	8.91	0.11	1.031	6.72	1 004
	•	•	AV =	1.002		AV :		1 1v =	0.996
	1		50 .	0.007		8D		8D =	6.021
				0.007			<u> </u>		0.021
High-density Oxide		<del></del>							
PEO - 381	313.00	612.98	1.19	1.000	632.46	1 39	1 032	622.72	1 016
PEO - 386	457 88	411.16	4.73	0.000	480.48	1.92	1 048	445 80	0 474
PEO - 447	778.46	729.55	2.10	1.030	832.11	1 09	1 072	815 83	1 051
LA0250C 10	69 80	44.37	1.46	0 742	56.60	2 34	0 981	51 53	0 862
PEO - 362A & LAO281C10	79.78	76 67	0.06	0 1 1	78 07	9.89	0.981	76 67	0 961
LA0251C10	171 43	89 84	4.12	6 2	173.72	9 65	1 013	121 62	0.768
LA0252C10	320 98	394.42	4 50	1.135	321.74	1 82	1 002	343.08	1 069
LAC253C10	611.04	729 78	3 82	1194	004.22	1 43	0 989	867.00	1 192
LAO201C11	874 10	911 65	4 44	1043	871.51	1 41	0 997	891.68	1 020
	-/- 10		Av .	0.047	1 0// 3/	A	1	Av e	0.979
			80 .			80		SD :	0.105
			- SU -	0.700	<b> </b>	80	· · · · · · · · · · · · · · · · · · ·	30 1	0.105
and Bied Ceugliles			···		<del></del>			<del></del>	
MPX -1826	134 26	102.84	0.31	0.786	178.24	1 22	1 328	140 54	1 047
MPX -1843	216 00	218.38	0.49	1013	263 08	1 90	1 216	240 98	1 116
MPX - 1907	222 81	185 14	0 24	0.741	284 77	2 44	1 2/8	224 95	1 010
MPX - 1945	63.70	52 84	0 39	U 630	88 85	8 9 8	1 081	60 65	0 955
MPX - 1986	124 00	109 90	0.61	0 888	186 72	3 27	1 256	134 81	1 071
MPX - 2190	100 00	188 32	0 23	0 936	172 21	1 60	1 037	103 77	0 987
MPX - 2240	136 00	133 78	0 20	0 984	193 53	1 64	1 129	143.07	1 056
MPX - 2298	294 00	109 95	0 20	0 3/4	504 98	1 65	710	307.48	1046
MPA - 2236	204 00	109 97			304 98				
			AV a	0.016 0.204	1	Av SD		Av n	1.036
					<del></del>				
Metten Belt Extraction									
XBLP - 121	186 37	148 49	0 30	0 950	238.79	9.75	1 537	148 49	0 956
XBLP - 276	00 30	00.00	0 30	0 951	121 63	12.28	1 346	05 89	0 951
XBLP - 301	246 96	23) 37	0 55	0 001	284 33	3 90	1 070	250 85	1 016
REMSE - 1	243 83	231 62	0 60	0 980	474 67	7 10	1 944	231.62	0 950
AFMSE - 2	372 73	384 80	0.71	0 982	780 74	4 /2	3 121	345 80	0 952
RFMBE - 4	400 80	197 89	1 31	0 974	897 34	5 90	2 196	397 69	0 974
ARF878886	203 50	286 74	1.05	0 870	483 97	4 21	1 /22	255 74	0 9/0
A(IF876842	219 80	202 70	1 31	0 023	107 43	0.45	1.756	202 70	0 973
	1	1	Av w	0.918	1	Av		Av »	0.002
			. 20	0.014	L	80		92 4	0 021
lavenneh filver In-plant filenderde				1				1	
KI:BIATI "BIADMATAA 4360	381 17	361 20		1 000	300 40		1.049	169 60	1 025
		0.7 0	0 01	, , , , ,					
4340	374 87	301 50	1 77	1 010	349 49		0 933	300 30	0.975
4301	113 42	112 20	1.08	0 989	114 67		1 011	113 44	1 000
4382	419 38	418 44	0 22	0 488	438 90		1 010	427 17	1 010
			Av =	1.001		Av		Av •	1.005
	l.	I	. 00	0.012	1	80	- 0.043 i	1 50 s	0.022

Samples prepared with philonium oxide and diatomaceous earth

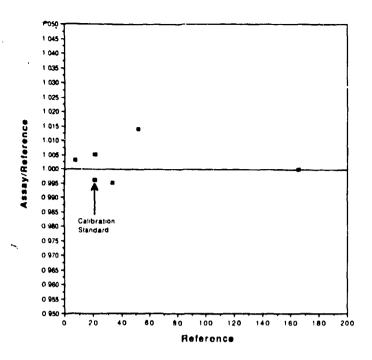


Fig. 1. Assay accuracy of the SGS for ash samples. These samples are uniform and of low density: well suited for SGS assay. The reference values are known to better than 1%.

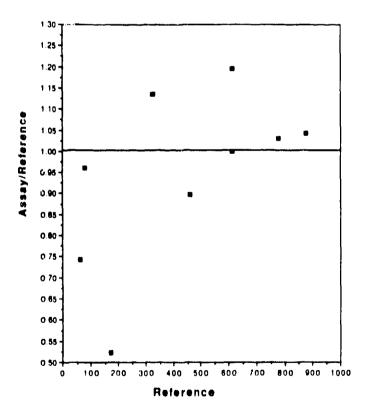


Fig. 2. Assay accuracy of the SGS for the plutonium oxide items. These pure, high density samples have well documented chemical compositions. The reference values are known to a few tenths of a percent.

The third set was the SSC samples generated in the pyrochemical process: residues from plutonium casting and broken crucible pieces. These samples are relatively high-density waste, with a low SNM mass heterogeneous in both the matrix and the plutonium. The high density makes the transmission measurement difficult. The plutonium content of each sample was determined by calorimetry and a gamma isotopic determination; for these samples the content should be accurate to 2%. Figure 3 shows the assay results of the SSC samples. The lump correction for these samples is large (as much as 60%). The SGS assay of these samples is 19% low while the NCC is 25% high. This indicates that the advanced SGS assay technique still has some bias although the bias is substantially reduced. It is interesting to note that if the average of the SGS and the NCC is used, it agrees with the reference values to 4% with an RSD of 5%. This follows the expected trend; SGS will assay low and the NCC will assay high. Consequently the combination brackets the true answer.

The fourth set of samples contains salts generated from the MSE process, in which americium and other impurities are extracted from the plutonium into the salts. The Am/Pu ratio in this salt is quite high (up to 5%) and the americium was physically separated from the plutonium before blending. We determined the plutonium content of these items by pulverizing them, removing metal lumps, blending the rest for an extended time, then taking multiple samples and analyzing them destructively. Chemical analysis was per ormed on different parts of the sample, and the agreement is between 1.5% and 2%. We feel that the plutonium content is known to 1.5%. Figure 4 shows the results of the SGS measurement of these samples. The SGS gives an average result 4% low, as compared with the reference values, with an RSD of 2.7%. These samples were measured by the SGS before pulverization; the

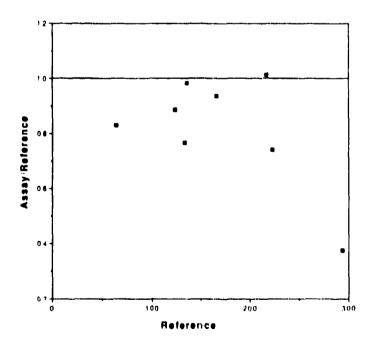


Fig. 3. Assay accuracy of the SGS for the SSC samples. These are noxious waste items not well suited for any measurement. They are heterogeneous and lumpy. The uncertainties in the reference values are about 2%.

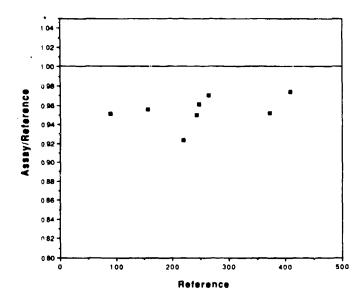


Fig. 4. Assay accuracy of the SGS for homogenized MSE salt scrap. These scrap items are prepared for sampling for chemical analysis to determine plutonium content. After preparation, they are suitable for SGS assay if a valid transmission measurement can be made. The uncertainties in the reference values are approximately 15%.

maximum lump correction is 15%. The NCC results are substantially higher than the reference values because of the high americium content; the  $(\alpha,n)$  neutrons are the dominant neutrons counted by the NCC. In fact the  $(\alpha,n)$  yield is so high that the samples have been measured using the self-interrogation technique.<sup>4</sup> These samples were flagged by the NCC reals-to-totals ratio test  $(R/T)^5$  as being unsuitable for the calibration curve and only the SGS values should be used for the assay result.

The fifth set of samples were fluoride contaminated process sweepings generated at Savannah River Site (SRS). These samples were characterized by calorimetry and gamma

isotopics. These measurements were performed at SRS. The LANL calibration was used on the SGS at SRS. The SGS measured the samples with an average bias 0.1% high and an RSD of 1.2%. The NCC had to be recalibrated with these standards because of the substantially different chemical form (fluoride vs oxide). The results of the SGS measurements can be seen in Fig. 5.

# CONCLUSION

This study shows that the advanced SGS can measure a wide range of material types and masses. We also showed that the SGS could be calibrated with one standard and still provide good results for a wide variety of samples. Figure 6 shows all of the measured values against the reference values for the various samples measured on the SGS.

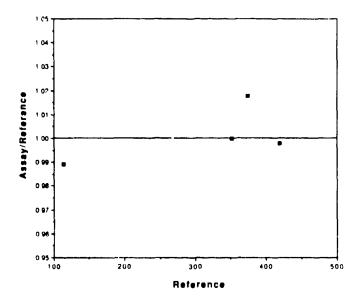


Fig. 5. Assay accuracy of the SGS for the in-plant scrap standards. These scrap items are from a working process. The uncertainties in the reference values are about 2%.

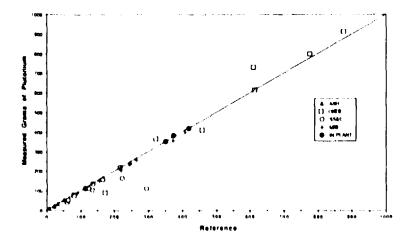


Fig. 6. Assay results of the SGS vs reference values for all of the standards measured.

If the scrap and waste can be separated according to density and material type, the SGS and the NCC can potentially perform assays with biases of less than 5% on some of the most difficult process samples to assay. The SGS and NCC complement each other and, if their results agree to within the uncertainties, we are reasonably confident of the assay result. When the results from both instruments do not agree, we have found it prudent to look at the data and examine the sample more carefully. Often the data from either instrument is obviously flawed. For example, the R/T ratio flag on the NCC may indicate the wrong calibration curve, or that the transmission in the SGS might be too low (<0.001) for a segment of the sample. Obviously, these results cannot be extrapolated to other sample types. These data demonstrate the need to evaluate each scrap and waste stream for measurement accuracy.

Our current efforts on the advanced segmented gamma-ray scanner are focused on improving the lump correction factor technique. We are also exploring the possibilities of making these measurements on SNM materials other than plutonium.

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